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INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification 6 : C09C 1/30, C08K 9/04		A1	(11) International Publication Number: WO 97/08250
			(43) International Publication Date: 6 March 1997 (06.03.97)
(21) International Application Number: PCT/EP96/03246		(81) Designated States: AL, AM, AT, AU, AZ, BB, BG, BR, BY, CA, CH, CN, CU, CZ, DE, DK, EE, ES, FI, GB, GE, HU, IL, IS, JP, KE, KG, KP, KR, KZ, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, TJ, TM, TR, TT, UA, UG, US, UZ, VN, ARIPO patent (KE, LS, MW, SD, SZ, UG), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG).	
(22) International Filing Date: 20 July 1996 (20.07.96)			
(30) Priority Data: 9517607.9 29 August 1995 (29.08.95) GB			
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(54) Title: SILICA PRODUCTS AND UV CURABLE SYSTEMS

(57) Abstract

Wax coated silica matting agent wherein the silica is an amorphous silica having a pore volume of at least 1.5 cm³/g, preferably at least 1.8 cm³/g, the wax coating being present in the range from 6 % to 15 % by weight of the matting agent and comprising a synthetic polyethylene wax.

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- 1 -

SILICA PRODUCTS and UV CURABLE SYSTEMS

FIELD OF INVENTION

5 The invention relates to wax coated silica matting agents used in the matting of UV curable systems and to UV curable systems containing the same.

BACKGROUND TO THE INVENTION

10 UV curing is based on photoinitiated polymerisation of functional oligomers and monomers into a crosslinked polymer network. When an ultraviolet curable coating is exposed to UV energy in this way a relatively hard film, having an 15 extremely smooth surface, and hence one of high gloss, is produced. With the increasing popularity of radiation cured coatings for a wide variety of applications, the ability to control and reduce gloss is becoming more important. It is well known that matt surfaces provide the finished article 20 with a more elegant appearance and hide imperfections at the surface, particularly in wood, furniture and PVC flooring applications, and several different methods of reducing the gloss of UV curable coatings have been reported, for example the use of "dual cure" or "gradient intensity cure" 25 techniques, specific photoinitiators and non-silica type matting agents.

30 Traditional silica matting agents are conveniently used to reduce the gloss of solvent and water based finishes and in the UV industry synthetic silicas are used to provide a semi-gloss or matt effect, although as a rule high concentrations are generally required by the formulator. The high solids nature of UV systems and the absence of 35 adequate film shrinkage, required to ensure optimal levels of particles are present in the surface of the cured film,

- 2 -

makes efficient matting difficult. Accordingly, high concentrations of conventional silicas are required to achieve an acceptable degree of gloss reduction. Such high levels of silica can frequently cause changes in the 5 rheological properties of the lacquer which can be detrimental to the coating and curing process and, can impair the optical properties of the cured film.

In an attempt to overcome this problem, the use of large 10 particle size silicas has been promoted in the past for both thin and thick film applications. Such materials may produce an unacceptable level of roughness particularly in thin coatings and, depending on the viscosity of the system, can result in a greater tendency to settle on prolonged 15 storage. It would be desirable therefore to provide a synthetic silica matting agent for UV systems, having good efficiency and minimal effect on formulation viscosity and film properties.

20 There is therefore a need for a new matting agent which overcomes these problems.

Definitions and Test Procedures

25 i. Nitrogen surface area - pore volume

Nitrogen surface area is determined by standard 30 nitrogen adsorption methods of Brunauer, Emmett and Teller (BET) using a multi point method with an ASAP 2400 apparatus supplied by Micromeritics of the U.S.A.. The samples are outgassed under vacuum at 270°C for at least one hour before measurement. Surface area is calculated from the volume of nitrogen gas adsorbed at p/p₀ 0.98. This apparatus also provides the pore size 35 distribution from which it is possible to get the pore

- 3 -

size (D_{10}) for which 10% of the pores are below this pore size. In the same manner, it is possible to get the pore size for which 50% (D_{50}) and 90% (D_{90}) of the pores are below this pore size. Additionally the pore volume (cm^3/g) for a given range of pore size can be obtained from the desorption curve.

ii. Matting efficiency in UV systems

10 In order to test the matting efficiency, two commercial
UV curable systems have been chosen for the study, one
is a urethane acrylate formulation (Formulation 2) and
one is representative of an epoxy acrylate formulation
(Formulation 1), details of which are given in the
15 following Table.

Formulation 2	%	Formulation 1	%
Ebecryl 294	62.1	Ebecryl 608	44.7
N-vinyl pyrrolidone	9.5	OTA 480	22.2
2-ethyl hexyl acrylate	19.2	TPGDA	22.2
Benzophenone	2.85	Benzophenone	3.3
Darocur 1173	0.95	Irgacure 651	2.2
Silica matting agent	5.4	Silica matting agent	5.4

30 For the preparation of the formulations the following procedure was adopted. The binder and diluent were added to a 60ml amber glass jar and stirred at 8000rpm for 1 minute using an IKA Ultra Turrax T25 homogeniser.

- 4 -

The remaining additives and silica were then combined by hand stirring, followed by dispersion at 8000rpm for one minute. The systems were allowed to deaerate and then drawn onto black glass plates using either a 12 5 micron (Formulation 1) or a 40 micron bar applicator (Formulation 2). The plates were cured on a single pass, in line with normal industrial practice, under a Fusion H-bulb (mercury lamp, 120 W/cm) using a line speed of 3.5 metres/minute. The glossmeter 10 readings at 60° (gloss) and 85° (sheen) were measured, by a BYK multiglossmeter.

iv. Weight mean particle size

15 The weight mean particle size is determined with the aid of a Malvern Mastersizer using 100mm path length lens. This instrument, made by Malvern Instruments, Worcestershire uses the principle of Fraunhoffer diffraction utilising a low power He/Ne laser. Before 20 measurement the sample was dispersed ultrasonically in water for a period of 7 minutes to form an aqueous suspension. The Malvern Mastersizer measures the weight particle size distribution of the silica. The weight mean particle size (d_{50}), the 10 percentile (d_{10}) 25 and the 90 percentile (d_{90}) are easily obtained from the data generated by the instrument.

v. Wax content of the coated silica

30 The carbon content of the coated silicas is determined by a Leco HF 100 induction furnace and Leco CS 244 Carbon analyser. The carbon present is converted to carbon dioxide at high temperatures using the induction furnace. The gas is then detected by an infra-red

- 5 -

detection system. The wax content (in % w/w) is calculated from the carbon level obtained.

GENERAL DESCRIPTION OF THE INVENTION

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It is a first object of the present invention to provide a wax coated silica matting agent characterised in that the silica is an amorphous silica having a pore volume of at least 1.5 cm³/g, preferably at least 1.8 cm³/g, the wax coating being present in the range from 6% to 15% by weight of the matting agent and comprising a synthetic polyethylene wax having a melting point of less than 85°C, preferably less than 80°C.

10

15 Preferably, the wax coating being is in the range from 10% to 15% by weight of the matting agent when the amorphous silica has a pore volume of less than 2.5 cm³/g.

20

It is a second object of the present invention to provide a UV curable system comprising 3 to 15% by weight of a matting agent wherein the mating agent is a wax coated silica, the silica being an amorphous silica having a pore volume of at least 1.5 cm³/g, preferably at least 1.8 cm³/g, the wax coating being present in the range from 6% to 15% by weight of the matting agent and comprising a synthetic polyethylene wax having a melting point of less than 85°C, preferably less than 80°C.

25

30 The wax coated silica matting agents are manufactured by a process that simultaneously melts the wax and comminutes the silica to the desired particle size distribution. Such a process is most effectively carried out in a fluid energy mill or microniser. The operating temperature can then be varied according to the requirements of the wax. The inlet temperature of the air being supplied to the fluid energy

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- 6 -

mill must be high enough to ensure the wax melts within the residence time profile of the milling equipment.

SPECIFIC DESCRIPTION OF THE INVENTION

5

The present invention which will be further described in the following examples.

10 Various silicas were coated with different waxes using the following process.

15 Blends of silica feedstock and the appropriate wax (of particle size similar to that of the amorphous silica) were fed to an AFG 200 fluid bed mill (supplied by Alpine AG, Augsburg, Germany), operating at an air inlet temperature of 180°C., the classifier speed and feed rate being set commensurate with obtaining a micronised product with a weight mean particle size in desired range.

20 Amorphous coated silicas having the following characteristics were produced.

- 7 -

	PV (*) (cm ³ /g)	APS (**) (μm)	Coating	Wax content (%)
Ex. 1	1.2	8.4	None	
Ex. 2	1.2	8.8	Ternary blend (1)	10.0
Ex. 3	1.2	8.7	Microcrystalline (2)	11.4
Ex. 4	1.2	8.2	Polyethylene (3)	6.0
Ex. 5	1.2	8.1	Polyethylene (3)	11.4
Ex. 6	1.8	9.2	Microcrystalline	13.2
Ex. 7	1.8	7.2	Microcrystalline	8.7
Ex. 8	1.8	6.9	Ternary blend	14.8
Ex. 9	1.8	6.7	Polyethylene (3)	6.0
Ex. 10	1.8	7.2	Polyethylene (3)	11.6
Ex. 11	1.8	7.4	Polyethylene (4)	11.1
Ex. 12	1.8	8.0	Polyethylene (5)	12.9
Ex. 13	1.8	7.4	Polyethylene (6)	12.2
Ex. 14	1.8	7.3	Polyethylene (7)	10.4
Ex. 15	2.5	9.0	Polyethylene (3)	5.6
Ex. 16	2.5	8.3	Polyethylene (3)	13.4
Ex. 17	2.5	3.9	Polyethylene (3)	12.3
Ex. 18	2.5	7.7	Microcrystalline	8.1

20

(*) Pore volume of the uncoated amorphous silica

(**) Average Particle Size of the coated silica

- 8 -

- (1) as disclosed in EP-A-541,359
- (2) obtainable from Petrolite under the tradename Crown 700
- (3) obtainable from Petrolite under the tradename Polywax 400 (melting point 79.5°C)
- 5 (4) obtainable from Petrolite under the tradename Polywax 500 (melting point 88°C)
- (5) obtainable from Petrolite under the tradename Polywax 655 (melting point 99°C)
- 10 (6) obtainable from Petrolite under the tradename Polywax 1000 (melting point 113°C)
- (7) obtainable from Petrolite under the tradename Polywax 2000 (melting point 126°C)

15 Then the matting efficiency at 60° and 85° was measured for the two formulations 1 & 2. The results are summarized in the following table, a low number indicates a good matting effect.

- 9 -

	Formulation 1		Formulation 2		
	60°	85°	60°	85°	
5	Ex.1	85	96	86	100
	Ex.2	82	90	85	96
	Ex.3	83	97	80	95
	Ex.4	91	95	81	94
	Ex.5	88	98	85	96
	Ex.6	88	90	84	90
	Ex.7	80	95	85	96
	Ex.8	88	90	78	95
10	Ex.9	91	93	75	93
	Ex.10	54	93	9	32
	Ex.11	77	98	57	92
	Ex.12	89	101	75	90
	Ex.13	88	99	82	99
15	Ex.14	88	96	83	97
	Ex.15	60	95	27	79
	Ex.16	57	98	13	55
	Ex.17	71	98	20	76
	Ex.18	91	92	83	90

20

As it can be seen, only examples 10, 15, 16 and 17 present good matting properties.

25

From examples 1 to 5, it can be seen that irrespective of the coating which is used, no satisfactory matting

- 10 -

properties are obtained. Examples 1 to 5 are characterized by a pore volume of 1.2 cm³/g.

In examples 6 to 14 (pore volume of 1.8 cm³/g), only example 10 gives satisfactory matting properties whereas the only difference between example 10 and example 9 is the wax content of the silica, proving at a pore volume of 1.8 cm³/g, a wax content of 6% is not enough to give the desired matting properties.

10

In examples 10 to 14 (various polyethylene wax types), only example 10 gives satisfactory matting performance, proving that the type of polyethylene wax, as defined by its melting point, is critical.

15

In examples 15 to 18 (pore volume of 2.5 cm³/g), examples 15 to 17 gives satisfactory matting properties, even at low loading (example 15), whereas example 18, even though at 8.1% loading does not give the required properties.

- 11 -

CLAIMS

1. Wax coated silica matting agent characterised in that the silica is an amorphous silica having a pore volume of at least 1.5 cm³/g, preferably at least 1.8 cm³/g, the wax coating being present in the range from 6% to 15% by weight of the matting agent and comprising a synthetic polyethylene wax.
- 10 2. Wax coated silica according to claim 1 wherein the amorphous silica has a pore volume of less than 2.5 cm³/g, the wax coating being present in the range from 10% to 15% by weight of the matting agent.
- 15 3. Wax coated silica according to claim 1 or 2 wherein the amorphous silica has a matting efficiency of below 20 gloss units at an incidence angle of 60° and a loading of 5.4% by weight in the urethane acrylate formulation (2).
- 20 4. Wax coated silica according to claim 1 wherein the synthetic polyethylene wax has a melting point of less than 115°C, preferably less than 100°C, more preferably less than 85°C.
- 25 5. UV curable system comprising 3 to 15 % by weight of a matting agent wherein the mating agent is a wax coated silica, the silica being an amorphous silica having a pore volume of at least 1.5 cm³/g, preferably at least 1.8 cm³/g, the wax coating being present in the range from 6% to 15% by weight of the matting agent and comprising a synthetic polyethylene wax having a melting point of less than 85°C, preferably less than 80°C.

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INTERNATIONAL SEARCH REPORT

Intern. Application No
PCT/EP 96/03246

A. CLASSIFICATION OF SUBJECT MATTER
IPC 6 C09C1/30 C08K9/04

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 6 C08K C09C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP,A,0 541 359 (CROSFIELD JOSEPH & SONS) 12 May 1993 see page 3, line 6 - line 8 see claims 1-3	1-5
A	US,A,4 097 302 (COHEN HOWARD JOSEPH ET AL) 27 June 1978 see claims 1-3	1-5

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

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Date of the actual completion of the international search 14 October 1996	Date of mailing of the international search report 25.10.96
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Information on patent family members

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Patent document cited in search report	Publication date	Patent family member(s)		Publication date
EP-A-0541359	12-05-93	AT-T-	125283	15-08-95
		CA-A-	2082035	08-05-93
		DE-D-	69203570	24-08-95
		DE-T-	69203570	01-02-96
		US-A-	5326395	05-07-94
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